

#### Simulation of Dam Breaking Phenomena in Accordance with Dimensional Analysis by DualSPHysics

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# Outline

- Dimensional Analysis and Similitude
- Similarity and Scaling Laws
- Simulation of Dam-Breaking by DualSPHysics
- Validation by Experimental Results



# **Dimensional Analysis**

Solutions of some real flow problems depend heavily on experimental data.

- To save time and money, tests are performed on a geometrically scaled model, not on the full-scale prototype.
- Experimentation on model must be properly scaled so that results are meaningful for the full-scale prototype.
- Thus, a technique called *dimensional analysis* is needed.



## Similitude or similarity

Similitude is defined as the similarity between the **model** and **prototype** in every aspect, which means that the model and prototype have similar properties.

- Geometric Similarity  $\lambda = \frac{L_{\rm m}}{L_{\rm rl}}$
- Kinematic Similarity  $\lambda_{\rm V} = \frac{v_{\rm m}}{V_{\rm rl}}$
- Dynamic Similarity

 $\lambda_{\rm F} = \frac{F_{\rm m}}{F_{\rm rl}}$ 

From geometric and velocity ratios other scales can be derived for time, accelerate, etc.

$$\lambda_{\rm t} = \frac{L_{\rm m} / V_{\rm m}}{L_{\rm rl} / V_{\rm rl}} = \frac{\lambda}{\lambda_{\rm V}}$$



oude numbers are the same corresponding val (a) prototype; (b) model.



# Model Analysis

- In a close conjunction or as a support to numerical simulation.
- Idealized laboratory models to calibrate or validate numerical simulation.
- Quality of experimental data strongly depends on measurement technique.
- The physical model must be designed in accordance with the corresponding scaling laws.





(b)

Example of model experiments (a) wind-tunnel (b) Spillway



Any hydraulic phenomena can be supposed as having a functional dependence of dimension variables of the type:

 $F_D(\rho,\mu,\sigma,K,L,V,\Delta P,g) = 0$ 

Application of Buckingham  $\pi$  theorem leads to an equivalent non-

dimensional relation of the form:

$$F_{\rm ND}\left(\frac{V}{\sqrt{gL}}, \frac{\rho VL}{\mu}, \frac{\rho V^2 L}{\sigma}, \frac{\Delta P}{\rho V^2}, V\sqrt{\frac{\rho}{K}}\right) = 0$$



#### **Dimensionless Groups in Fluids**

1.	Froude number = $\frac{inertia \ force}{gravity \ force}$	$\mathrm{Fr} = rac{V}{\sqrt{gL}}$
2.	Reynolds number = $\frac{inertia \ force}{viscouse \ force}$	$\operatorname{Re} = \frac{\rho VL}{\mu} = \frac{VL}{v}$
3.	Weber number = $\frac{inertia \ force}{surface \ tension \ force}$	We = $\frac{\rho V^2 L}{\sigma}$
4.	$Euler number = \frac{pressure \ force}{inertia \ force}$	$\mathrm{Eu} = \frac{\Delta P}{\rho V^2}$
5.	Mach number = $\frac{inertia \ force}{compressibility \ force}$	$Ma = V \sqrt{\frac{\rho}{K}}$



## **Dimensionless Numbers for Dam Breaking**

- Froude law  $Fr_p = Fr_m$  implies:  $\lambda_v = \lambda_t = \lambda^{1/2}$
- ~ Free surface flow, gravity-dominant flow
- ~ Compressibility and surface tension may be ignored
- Reynolds law  $Re_p = Re_m$  calls for:  $\lambda_v = \lambda^{-1}\lambda_v$
- ~ Viscosity-dominant flow
- ~ Low-speed problem



# Combined Action of Gravity and Viscosity

Dam breaking problem requires both Froude similarity and Reynolds similarity.

$$Fr_{p} = Fr_{m} = \left(\frac{v}{\sqrt{g l}}\right)_{p} = \left(\frac{v}{\sqrt{g l}}\right)_{m} \rightarrow \frac{V_{m}}{V_{p}} = \sqrt{\frac{g_{m}}{g_{p}}}\frac{l_{m}}{l_{p}}} \quad (a)$$

$$Re_{p} = Re_{m} = \left(\frac{V l}{v}\right)_{p} = \left(\frac{V l}{v}\right)_{m} \rightarrow \frac{V_{m}}{V_{p}} = \frac{v_{m}}{v_{p}}\frac{l_{p}}{l_{m}}} \quad (b)$$
For  $g_{m} = g_{p}$ 

$$\frac{v_{m}}{v_{p}} = \left(\frac{l_{m}}{l_{p}}\right)^{1.5} \rightarrow v_{m} = v_{p} / \left(\frac{l_{m}}{l_{p}}\right)^{1.5} \quad (c)$$

$$f \quad \frac{l_{m}}{l_{p}} = \frac{1}{10} \rightarrow v_{m} = \frac{v_{p}}{31.6} \quad \text{water:} \quad \mu = 1.0 \times 10^{-3} \text{ Pa} \cdot \text{s} \quad \text{Hydrogen:} \quad \mu = 0.21 \times 10^{-4} \text{ Pa} \cdot \text{s}$$

- A liquid of appropriate viscosity must be found for the model test.
- If same liquid is used, then model is as large as prototype.



# **Dam-Breaking Numerical Model**

- A liquid of appropriate viscosity cannot be found for the dam breaking test.
- It is not usually possible to have a model as large as prototype.
- It is impossible to keep Froude and Reynolds numbers in the model equal to those in prototype.
- A choice between the Froude and Reynolds numbers should be made in experimental model.

Physical model can be replaced by NUMERICAL MODEL in order to satisfy both

Froude law and Reynolds laws in the tests.



#### Dam Breaking Prototype by G. Gesteira, (2004)

- A 160 cm long, 61 cm wide, and 75 cm high box.
- Velocity measurement by a laser Doppler velocimetry (LDV) system.
- Velocity measurement at 754, 310, and 26 mm.
- 1.5 s physical time of prototype.





## Dam Breaking Model by DualSPHysics



 $u_p = 1e - 6$  dynamic viscosity of prototype fluid (water)  $u_m = 3.53e - 7$  dynamic viscosity of model fluid (artificial fluid)





#### Simulation Set up in DualSPHysics

Run	Inter-particle distance (IDP)	IDP to height ratio	Number of particles (NOP)	Physical time (s)	Kinematic viscosity (m2/s)	Run time (h)
1	8 mm	0.053	29716	1.06	3.5 e −7	2
2	7 mm	0.046	42988	1.06	3.5 e −7	3.5
3	6 mm	0.04	64457	1.06	3.5 e −7	6
4	4 mm	0.026	207754	1.06	3.5 e −7	30

- IDP to height ratio higher than 0.053 produces unrealistic results.
- Higher computational time than high viscosity fluids.
- 1.06 s of simulation time is equivalent to
  1.5 s of physical time.





#### Validation by Experimental Data of G. Gesteira (2004)





# Simulation of Dam Breaking

Run	Inter-particle distance (IDP)	IDP to height ratio	Number of particles (NOP)	Fluid particles	Physical time (s)	Shifting algorithm	Kinematic viscosity (m2/s)	Run time (h)
1	4 mm	0.0266	207754	142500	1.06	No	3.5 e −7	30
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		V	el Maanitude					
	5 8950-0	3 005	10 2	8 37910+00				
	0.0700-0.							
	4							
4	××							

 Reduced scale to save computational time.

- Same Froude number and Reynolds number.
- High accuracy results.